

MEASUREMENT OF SHIP'S MOTIONS

The *ELECTROLEVEL* is an electronic gravity sensing transducer which can be used in various configurations to measure the motions of a ship at sea. This application note examines the accuracy of such measurement and discusses the background to measuring ships motions.

A ship at sea is subject to six oscillating motions:

Pitch angular motion about the ships transverse axis.
Roll: angular motion about the ships longitudinal axis.
Yaw: angular motion in the horizontal plane containing the

projection of the longitudinal axis, about the mean course.

Surge: fore and aft movement of the C.G. of the ship after

subtracting mean speed.

Sway: transverse movement of the C.G. of the ship

measured in the horizontal plane.

Heave: vertical movement of the C.G. of the ship.

These motions are produced by wave action and evidently depend on the heading and size of the ship with respect to the waves.

Because the *ELECTROLEVEL* is pendulous device it senses accelerations as well as gravity. These accelerations cause errors in angular reading.

The magnitude of these errors is examined in the following analysis in which a simple model of ships motion is used to identify the chief causes of error in practical situations.

Mathematical Analysis

Consider an **ELECTROLEVEL** sensor mounted on board ship at a height h and lateral displacement b from the axis of a rolling motion represented by

 $qr=q_1 \sin wt$ (see fig. 1).

The polar coordinates of the sensor are \mathbf{R} \mathbf{q} , and the corresponding cartesian coordinates are $\mathbf{X} = \mathbf{R} \sin \mathbf{q}$ $\mathbf{Y} = \mathbf{R} \cos \mathbf{q}$

where q=q0+q1 sin wt

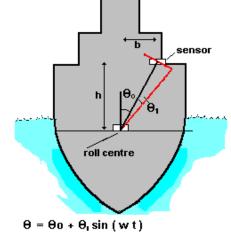


Figure 1

An $\it ELECTROLEVEL$ subject to accelerations $\it x$ " , $\it y$ " produces an output which is interpreted as an effective angle $\it q_{\it eff}$

(see application note *ELECTROLEVEL* AS AN ACCELEROMETER).

where $q_{eff}=q_{true}$ - arctan(x''/(g+y''))

After some reduction neglecting terms q_1^3 and smaller,

error angle= $+q_1(1+hw^2/g) \sin(wt) + bw^2/g$. $q_1^2 \cos(2wt) - (hb/g^2)w^4q_1^2 \sin^2(wt)$

From this equation we can draw the following practical conclusions:-

To measure static angles, e.g. trim, heel or alignment angles, a time constant filter circuit will reduce the first two error terms to an arbitrarily small value, at the expense of a slower response time

(see application note TIME CONSTANT IN *ELECTROLEVEL* CIRCUITS).

However the third term has a non-zero d.c. error value of ½(hb/g²)w⁴ q₁² which will not be attenuated by any filter method.

If **b** and **h** can be chosen near zero i.e. by mounting the *ELECTROLEVEL* sensor near the pitch and roll centre of the vessel, all acceleration errors can be reduced. If this mounting position is not possible, then equation 1 gives an estimate of the error, (which is negligible for many applications.)

E.g. for a 6° roll amplitude with 10 second period the d.c. error term is 1.6 arc seconds per metre² of displacement.

So if h = b = 10 metres the resulting datum error caused by these acceleration effects is approximately 3 minutes of arc.

To measure dynamic angles - e.g. pitch and roll amplitudes such as $\mathbf{q_1}$ equation 1 shows the values of h, b must be reduced to low level by mounting the sensor at the pitch and roll centre of the vessel.

If this is not possible then the error terms in equation 1 can be reduced by taking readings from an array of suitably placed sensors and computing the true angle of roll.

Fig 2 shows such an arrangement where the roll centre of the ship is inaccessible.

Two sensors are mounted at heights h_a h_b above the roll centre (where b=0)

The measured angles are thus:

$$q_a = q_1 (1+h_a w^2/g) \sin (wt)$$

$$q_b = q_1 (1+h_b w^2/g) \sin(wt)$$

And the combination

$$(h_b q_a - h_a q_b)/(h_b - h_a) = q_1 \sin(wt)$$

is the true roll angle.

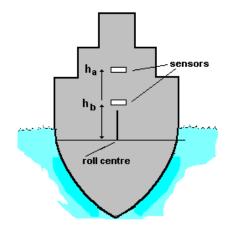


Figure 2

Note that error cancellation is frequency independent and hence applies for any oscillatory roll motion experienced by the ship.

Practical limits to error cancellation techniques like this are determined by

- (a) flexure of the ship
- (b) the matching of the two sensor characteristics over their operating range. (This can be made quite close by selecting the sensors.)
- (c) third order effects caused by coupling of surge, yaw, heave and sway motions.

Dynamic response of the ELECTROLEVEL

To a first approximation the ELECTROLEVEL behaves like a simple pendulum with a natural frequency of oscillator \mathbf{w} and damping factor \mathbf{d} . The natural frequency of the standard ELECTROLEVEL sensors is between 1 and 2.5 Hz and is ideally suited to following low frequency wave-induced motion. The damping factor \mathbf{d} . is between 0.6 and 0.9 at room temperature. Exceptionally, for a very small vessel a correction might have to be made for higher frequency oscillations

Summary and Miscellaneous Comments

The most effective method of measuring true roll and pitch angles on board ship is to

- (a) Mount the transducer at the centre of minimum pitch movement.
- (b) If this is not possible then to mount the sensor in the same horizontal plane as the pitch/roll centre so that h=0.
- (c) Failing a, b, use two transducers at different heights and an error compensation circuit to remove acceleration terms.

Note that it is possible to measure the linear acceleration terms, heave surge and sway with accelerometers and to electronically double integrate these terms to give a reading of displacement.

Note also that in some applications concerned with stability of on deck loads, etc., it can be desirable to mount the *ELECTROLEVEL* sensors at the load location, since there they will give an *apparent pitch/roll* reading directly related to the inertial forces causing load instability, (see for example APPLICATION NOTE: DECK MOVEMENT INDICATOR).

Our engineering staff are always pleased to discuss an individual application in detail and to provide proposals for suitable equipment.

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